

Harmonic Suppression In Microstrip Dual-Mode Ring-Resonator Bandpass Filters

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Abstract

This paper introduces two new topologies for rejecting the harmonics in microstrip ring resonator filters. First one uses 50 Ω spur line filter structures placed at the input and output of the ring to suppress the first harmonic. Second topology incorporates low-pass structures into the ring for elimination of the harmonics.

Introduction

Wu and Rosenbaum [1] indicated the possibility that the TM₁₁₀ resonance, using their mode definitions, could be excited twice on the same physical ring thereby creating a dual-mode microstrip ring resonator. This feature of the microstrip ring is similar to the dual-mode resonator in cylindrical waveguide, which is extensively used in filter design. Wolff [2] presented experimental evidence of the excitation of the degenerate modes. The realisation of microwave filters using dual-mode ring resonators was first presented by Guglielmi and Gatti [3] at the 1990 European Microwave Conference. The technique is particularly attractive because of its ability to implement two transmission poles and two transmission zeroes with only one ring if a 'symmetric' coupling structure is employed. The technique is especially suitable for realising small light-weight filters for space applications. The possibility of enhancing this technique by using simple geometry to make the circuit less sensitive to fabrication tolerances and easier to simulate accurately has been demonstrated by [4]. This 5.4 GHz 2-pole planar filter, measuring only 15x15 mm, had a bandwidth of 300 MHz, with 1 dB insertion loss and high selectivity. However, due to the higher order resonances of transmission-line ring resonators the out-of-band rejection of the filter needs to be improved. This paper introduces two new topologies for rejecting this higher order resonances without disturbing the passband specifications.

The Spur-line Band-stop Filter

Bates [5] designed a microstrip spur-line band-stop filter suitable for bandwidth of the order of 10% within the width of a microstrip transmission line as shown in figure 1. The length of the spur a and the gap b determine the centre frequency f_0 given by:

$$a = \frac{2.997925 \cdot 10^8}{4 f_0 \sqrt{K_{effo}}} - \Delta l_l \quad (1)$$

Where K_{effo} and Δl_l are the odd-mode effective dielectric constant and the effective length extension due to the gap b respectively. This filter forms a compact structure that is also virtually nondispersive. The behaviour of this filter can be represented by means of an impedance matrix, derived by Jones and Bolljahn [6]. In Bates' analysis, which includes the effect of the capacitance between the end of the spur and the main line, the energy stored by the resonant structure was found to be mainly determined by the odd mode of propagation. It is well known that the microstrip propagation is not TEM and therefore the phase velocities for the odd and even mode are not equal; but assuming equal phase velocities the spur-line filter can be represented as the equivalent circuit given by Bates [5]. The band-stop spur-line filter was designed to operate at the first harmonic frequency of the ring filter. Taking advantage of its inherent space-saving nature, the spur-line filter was then embedded in both the input and output 50 Ω lines of the ring filter as shown in figure 2. When cascaded, the resulting topology produced a significant suppression of the first harmonic, where a comparison of the simulated transmission and return loss of the ring filter with and without the spur-line filter is shown in figure 3. Figure 4 shows the measured response of the spur line ring resonator filter it has 400 MHz 3dB bandwidth centered at 5.5 GHz and the second

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harmonic is suppressed successfully. Figure 5 shows the photograph of the spurline filter.

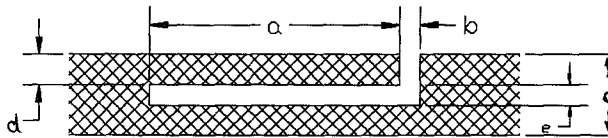


Fig. 1. Spur-line band-stop filter.

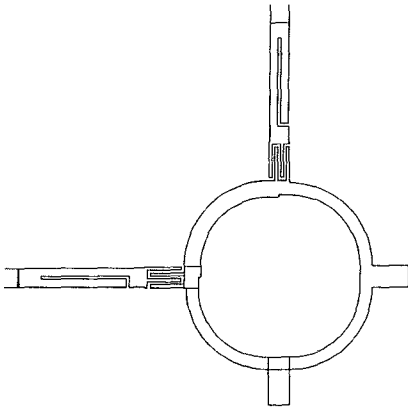


Fig. 2 Layout of the spur line ring resonator filter

Low-Pass Ring Structures

There are a three main ways in which a low-pass structure can be integrated into the rings for elimination of the unwanted higher frequency transmission bands:

- 1) using alternate sections of narrow and wide lines as shown in Fig. 6(a).
- 2) placing open circuit stubs on the ring to realise shunt capacitances Fig. 6(b)
- 3) placing radial stubs on the ring as shown in Fig. 6(c)

This structure can be termed a 'daisy' ring. With careful design a dual-mode ring without higher order resonances results. These behave as slow-wave structures and this leads to a further advantage which is that the size of the ring is reduced.

In principle, any of these three methods should work. However, the dual-mode ring is very sensitive to the symmetry and mode coupling discontinuities. Experimentally it has been found that method (1) gives the closest response to the normal ring.

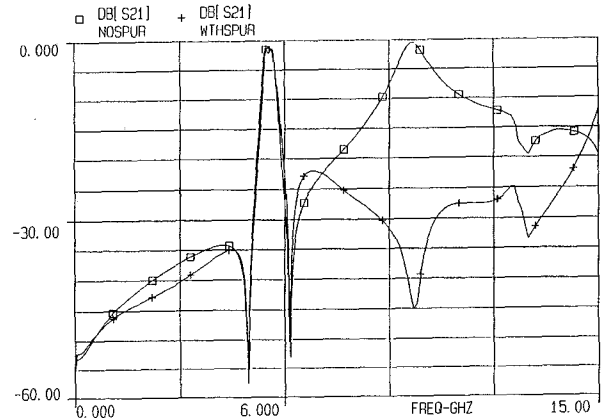


Fig. 3 Simulated response of the ring resonator filter with and without the spur line at the input and the output

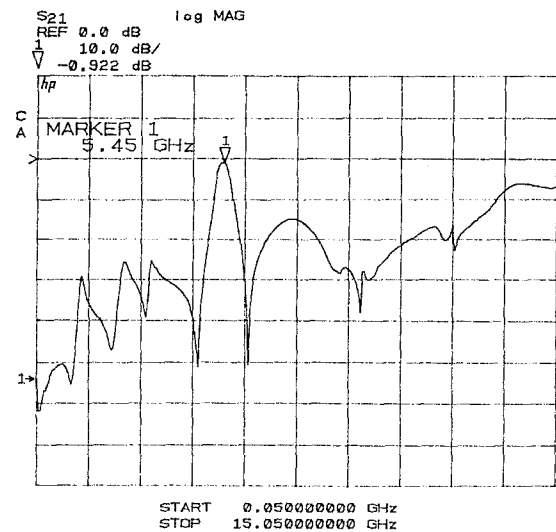


Fig. 4(a) Measured insertion loss of the spur line ring filter

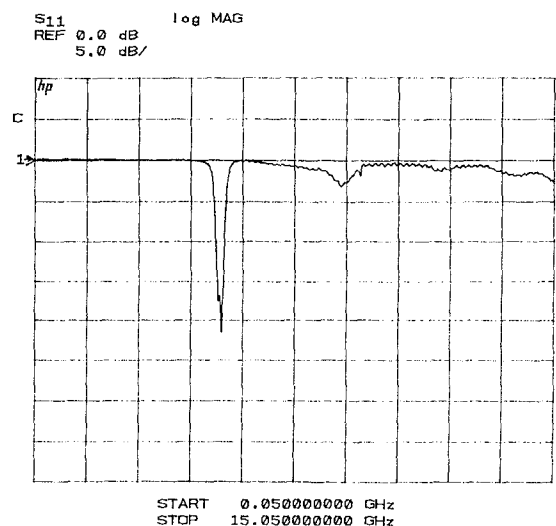


Fig. 4(b) Measured return loss of the spur line ring filter

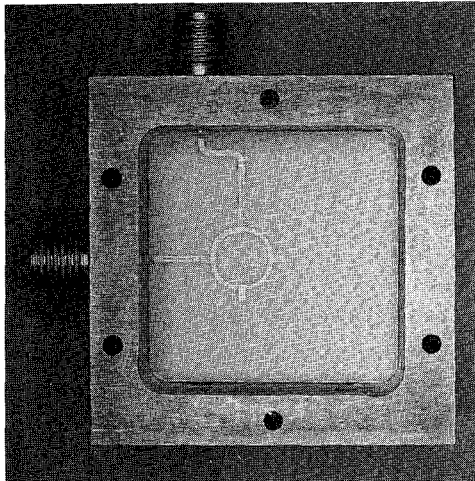


Fig. 5 Photograph of the spur line ring resonator filter

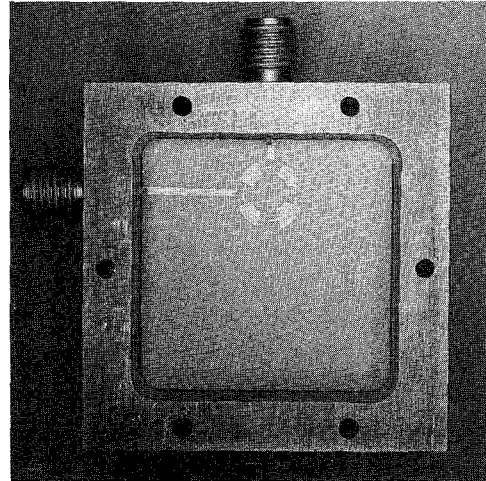


Fig. 7 Photograph of the dual-mode daisy ring filter

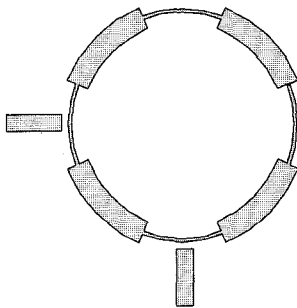


Fig. 6(a) Low-Z/
High-Z low-pass ring

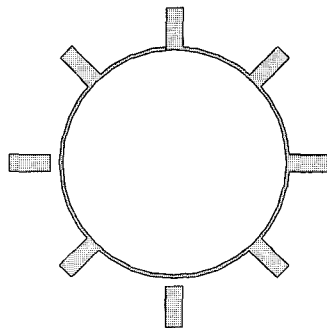


Fig. 6(b) Low-pass
ring with open circuit
stubs

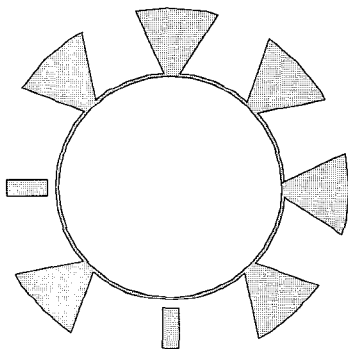


Fig. 6(c) Low pass
ring with radial stubs

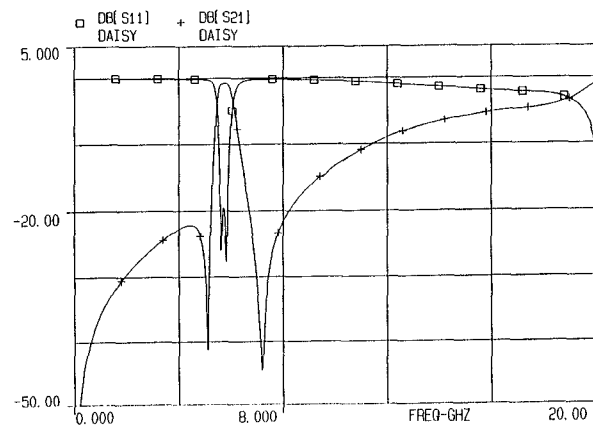


Fig. 8 Simulated response of the daisy ring filter

Measurements

A photograph of the finished dual-mode daisy ring filter is shown in Fig. 7. The pre-fabrication simulated response is shown in Fig. 8. The measured results of the filter are shown in Fig. 9. Absolutely no tuning was employed, and yet the agreement with predictions is excellent. The transmission response shows an excellent shape with a 500 MHz 3-dB bandwidth. Steep skirts are provided by the transmission zeros, and there are no spurious transmission bands from higher order resonances. The return loss response shows the positions of the two poles clearly. For comparison, Fig. 10 shows the measured response of a 5.25 GHz dual-mode ring filter which did not use the low-pass structure: The problem of the higher order resonances is very clear.

Conclusions

New techniques has been demonstrated for improving the out-of-band rejection of dual-mode microstrip ring resonator filters. A "daisy ring" 5.25 GHz filter prototype has been designed and constructed and gives a nearly ideal response. The measured results show a 3-dB bandwidth of 500 MHz centred on 5.25 GHz. The filter has steep skirts as a result of the transmission zeros given by the dual-mode ring and has greatly improved high frequency rejection compared with the standard dual-mode ring. However in the small space of the ring it is difficult to realise a low-pass filter structure with a sufficiently high order to filter the second resonance fully. the alternative method is to remove second resonance with a band-stop filter element. This has been successfully demonstrated by using a spur-line bandstop filter within the feedlines of the ring. This attenuates the second resonance by over 30dB, with no size penalty.

References

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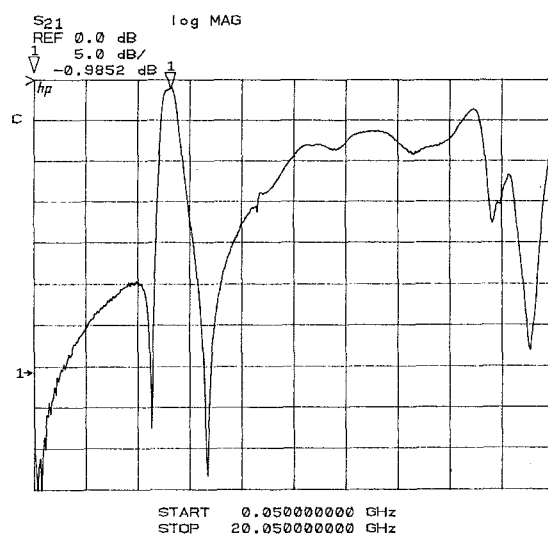


Fig. 9(a) Measured insertion loss of daisy ring filter

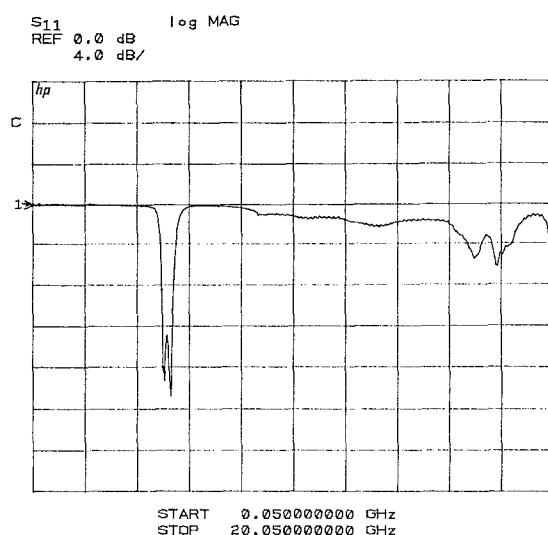


Fig. 9(b) Measured return loss of daisy ring filter

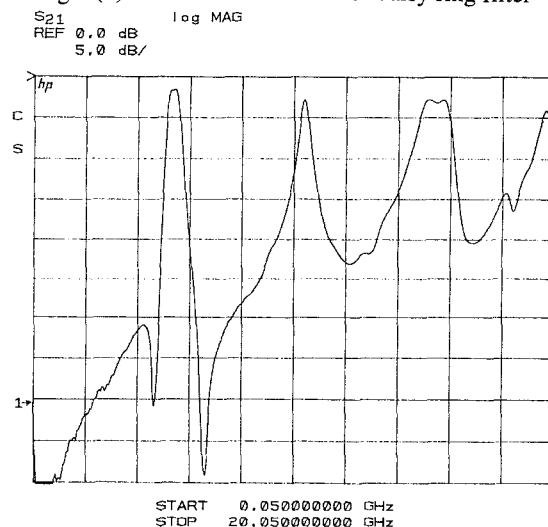


Fig. 10 Measured insertion loss of standard dual-mode ring